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A Two –Dimensional numerical Study of the effect of variable heat transfer coefficient on the performance of annular fins

Abstract

This work involves a numerical two-dimensional study on the effect of the variation in heat transfer coefficient on the performance of annular fins. The object was to study the effect of varying the heat transfer coefficient on the fin efficiency., Fin effectiveness, optimum length and the heat flow for fins of different cross-section, namely, constant thickness, and trapezoidal assuming a two dimensional flow inside the fin (radial and axial).

The results were obtained through setting up the governing equations and solving them by a finite difference technique employing the method of grid generation and coordinate transformation with the aid of the Gauss-Siedel method.

A power relationship was used to describe the variation of the heat transfer coefficient as a function of the fin length.

It was found that the variation in heat transfer coefficient reduces the fin efficiency, effectiveness, optimum length and the temperature gradient at the root of the fin and consequently the amount of heat transfer. Further more this variation led to an increase in the volume required to dissipate a known quantity of heat as compared to the constant coefficient case It was also found that heat dissipation increased with the increase in fin length to a certain limit and then begins to drop.

M		W	M2	ꝝ	ꝝ	ꝝ	Ar
		r,z	M2				Az
		ξ,η	M2				Ab
		η					F
		ε		ꝝ	ꝝ	ꝝ	FLOP
			W/m2k		ꝝ	ꝝ	H
	E	W/m2k		ꝝ	ꝝ		ha
	O				ꝝ		J
r	r,rr	W/m k					K
z	z,zz			ꝝ		ꝝ	Ka
r z	Rz	M			ꝝ		Lf
ξ	ξ,ξξ						M
ηξ	ηξ						N
η	η,ηη	W		ꝝ			Qcond.
		W		ꝝ			Qconv.
		W		ꝝ	ꝝ		Qf
		W		ꝝ	ꝝ	ꝝ	Qnf
		W					Qr
		W		ꝝ	ꝝ	ꝝ	Qr+Δr
		W					Qz
		W		ꝝ	ꝝ	ꝝ	Qz+Δz
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M							re
M							ro
M		ꝝ	ꝝ	ꝝ			RL
K/kw							Rs
K/kw							TR
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 \tilde{O} & \tilde{O} & & & & & \tilde{O} & \tilde{O} & \tilde{O} \\
 \tilde{O} & \tilde{O} & \tilde{O} & \tilde{O} & \tilde{U}\tilde{O} & & & \tilde{O} & \tilde{U}\tilde{O} \\
 \tilde{O} & \tilde{O} & \tilde{O} & \tilde{O} & & & & & \tilde{U} \\
 \tilde{O} & \tilde{U} & \tilde{O} & \tilde{O} & \tilde{U} & \tilde{U} & & \tilde{U} & \tilde{U} \\
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 & & & & & \tilde{U} & & & \tilde{U} \\
 & & & & & & [1] & &
 \end{array}$$

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$$\begin{array}{ccccccc}
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 \tilde{U} & \tilde{U} & \tilde{U} & \tilde{U} & \tilde{U} & \tilde{U} & \tilde{U} \\
 \tilde{O} & \tilde{U} & \tilde{U} & \tilde{U} & \tilde{U} & \tilde{U} & \tilde{U} \\
 \end{array}$$

$$\frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} + \frac{\partial^2 T}{\partial z^2} = 0.0 \quad . \quad \begin{array}{c} \text{(1)} \\ \text{(C.D)} \end{array} \quad [13] \quad \dots \quad (2)$$

$$\xi = \xi(r, z) \quad \dots (3)$$

$$\eta = \eta(r, z)$$

$$\frac{\partial}{\partial r} = \xi_r \frac{\partial}{\partial \xi} + \eta_r \frac{\partial}{\partial \eta} \quad \dots(4)$$

$$\frac{\partial}{\partial z} = \xi_z \frac{\partial}{\partial \xi} + \eta_z \frac{\partial}{\partial \eta} \quad \dots(5)$$

$$\frac{\partial T}{\partial \xi} = T_\xi \cdot \xi_r + T_\eta \cdot \eta_r \quad \dots(6)$$

$$\frac{\partial T}{\partial z} = T_\xi \cdot \xi_z + T_\eta \cdot \eta_z$$

$$\frac{\partial^2 T}{\partial r^2} = \xi_r^2 T_{\xi\xi} + 2\xi_r \eta_r T_{\xi\eta} + \eta_r^2 T_{\eta\eta} + \xi_{rr} T_\xi + \eta_{rr} T_\eta$$

... (7)

... (8)

$$\frac{\partial^2 T}{\partial z^2} = \xi_z^2 T_{\xi\xi} + 2\xi_z \eta_z T_{\xi\eta} + \eta_z^2 T_{\eta\eta} + \xi_{zz} T_\xi + \eta_{zz} T_\eta \quad \dots(9)$$

(2)

$$(\xi_r^2 + \xi_z^2)T_{\xi\xi} + 2(\xi_r\eta_r + \xi_z\eta_z)T_{\xi\eta} + (\eta_r^2 + \eta_z^2)T_{\eta\eta} + (\xi_{rr} + \xi_{zz})T_\xi + (\eta_{rr} + \eta_{zz})T_\eta + \frac{1}{r}(T_\xi\xi_r + T_\eta\eta_r) = 0.0 \quad (2)$$

$$T_{\xi\eta} T_\eta T_\xi T_{\eta\eta} T_{\xi\xi} \quad \dot{\cup} \quad (\quad) \quad (2)$$

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$$\begin{aligned} \frac{\partial T}{\partial z} &= 0.0 & U \\ \frac{\partial T}{\partial z} = T_\xi \cdot \xi_z + T_\eta \cdot \eta_z &= 0.0 & \dots(10) \end{aligned}$$

$$\eta_Z \quad T_\xi \tilde{O} \quad \tilde{O} \qquad \qquad \qquad r_\eta \quad T_\eta \quad \dot{U}$$

$$\frac{\partial T}{\partial r} = 0.0 \quad \dots(11)$$

$$\begin{array}{ccccccccc}
 \tilde{\text{O}} & \tilde{\text{O}} & \tilde{\text{O}} & \tilde{\text{O}} & . & T_{\xi}, Z_{\xi} & \tilde{\text{U}} & T_{\eta}, Z_r \\
 \tilde{\text{O}} & \tilde{\text{O}} & \tilde{\text{O}} & . & \tilde{\text{U}} & . & \tilde{\text{U}} & \tilde{\text{U}}
 \end{array}
 \quad (12)$$

$$S = \sqrt{dr^2 + dz^2} \quad \dots(12)$$

$$dr = r_\xi \cdot d\xi + r_\eta \cdot d\eta \quad \dots(13)$$

$$dz = z_\xi \cdot d\xi + z_\eta d\eta \quad \dots(14)$$

$$\begin{array}{ccccccccc} \tilde{O} & \tilde{O} & \tilde{O} & \tilde{O} & \eta & \tilde{U} & d\xi=1 & d & \eta=0.0 \\ dr = r_\xi & & & & & & & & \\ dz = z_\xi & & & & & & & & \\ \end{array} \quad \dots(13) \quad \dots(14), (13)$$

$$S_\xi = \sqrt{r_\xi^2 + z_\xi^2} \quad \dots(15)$$

$$(12) \quad \begin{array}{ccccccccc} \tilde{O} & \tilde{O} & \tilde{O} & \tilde{O} & \xi & \tilde{U} & d & \eta=1 & d\xi=0.0 \\ & & & & & & & & \\ & & & & & & & & \vdots \end{array}$$

$$S_\eta = \sqrt{r_\eta^2 + z_\eta^2} \quad \dots(16)$$

$$S_{\xi_2} = \sqrt{(r(i+1, j) - r(i, j))^2 + (z(i+1, j) - z(i, j))^2} \quad \dots(17)$$

$$S_{\xi_1} = \sqrt{(r(i, j) - r(i-1, j))^2 + (z(i, j) - z(i-1, j))^2} \quad \begin{array}{c} i+1 & i \\ \vdots & \\ j-1 & j \end{array} \quad \tilde{U} \quad \dots(18)$$

$$S_\eta = \sqrt{(r(i, j) - r(i, j-1))^2 + (z(i, j) - z(i, j-1))^2} \quad (i, j) \quad \dots(19)$$

$$Q_{\text{cond}} = Q_{\text{conv}} \quad \begin{array}{c} . \\ \tilde{O} \quad \tilde{O} \quad \tilde{U} \quad \tilde{O} \quad \tilde{O} \\ \vdots \end{array} \quad \begin{array}{c} \tilde{U} \\ \tilde{U} \end{array} \quad \dots(20)$$

$$\begin{array}{ccccccccc} \tilde{O} & \tilde{U} & \tilde{O} & & & \tilde{U} & \tilde{U} & & \\ & & & & & & & & \\ \tilde{O} & \tilde{U} \tilde{O} & \tilde{O} & \tilde{O} & & & & & \\ \tilde{O} & & \tilde{U} \\ & & & & & & & & \\ & & & & & & & & \dots[16] \\ & & & & & & & & \\ \tilde{O} & \tilde{O} & \tilde{O} & \tilde{O} & & \tilde{U} & \tilde{U} & \tilde{U} & \tilde{U} \\ & & (&) & & \tilde{U} & \tilde{U} & \tilde{U} & \tilde{U} \\ & & & & & & & & \\ & & & & & & & & : [3] \end{array}$$

$$h(r) = ha \cdot \frac{\left[\left(\frac{r_e}{r_o} + 1 \right) * (am + 1) * (am + 2) \right]}{2 * \left[(am + 1) * \frac{r_e}{r_o} + 1 \right]} * \left[\frac{(r - r_o)}{(r_e - r_o)} \right]^{am} \quad \dots(21)$$

$$\begin{array}{ccccccccc} \tilde{O} & (& \tilde{U} & \tilde{U} &) & \tilde{U} & \tilde{U} & & \\ & & \tilde{U} & \tilde{U} & & & & & \\ & & & & & & & & \tilde{U} \end{array}$$

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 (am=0.0) (am=1.0) (am=2.0) (ë)Ù Ù [3] Ù Ù Ù Ù Ù Ù Ù Ù Ù Ù Ù Ù Ù Ù Ù Ù
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$$R_L = \frac{\ln\left(\frac{r_e}{r_o}\right)}{2\pi k w} \quad \dots(22)$$

$$R_t = \frac{w}{4\pi k w} \quad \dots(23)$$

$$R_s = \frac{1}{2\pi ha(r_e^2 - r_o^2)} \quad \dots(24)$$

$$TR = \sqrt{R_L^2 + R_t^2} + R_s \quad \dots(25)$$

$$\frac{Q}{A} = \frac{\dot{m} \cdot h_f - \dot{m} \cdot h_i}{\dot{m} \cdot C_p} = \frac{\dot{m} \cdot (h_f - h_i)}{\dot{m} \cdot C_p} = \frac{h_f - h_i}{C_p}$$

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$$\eta = \frac{Q_f}{Q_{\max}} \quad \dots (26)$$

$$\mathcal{E} = \frac{Q_f}{Q_{nf}} \quad (27)$$

$$\dots(28) FLOP = \eta \cdot \varepsilon$$

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$$\begin{matrix} \hat{\mathbf{U}} & \hat{\mathbf{U}} & & \hat{\mathbf{U}} & & \hat{\mathbf{U}} \\ & & (2.0, 1.0, 0) & & , & , \\ \tilde{z} & & & & z & z \end{matrix}$$

(am = 0.0) . (am = 1.0) 2.0)
 (0.005m ,0.003m)

. (0.1m)

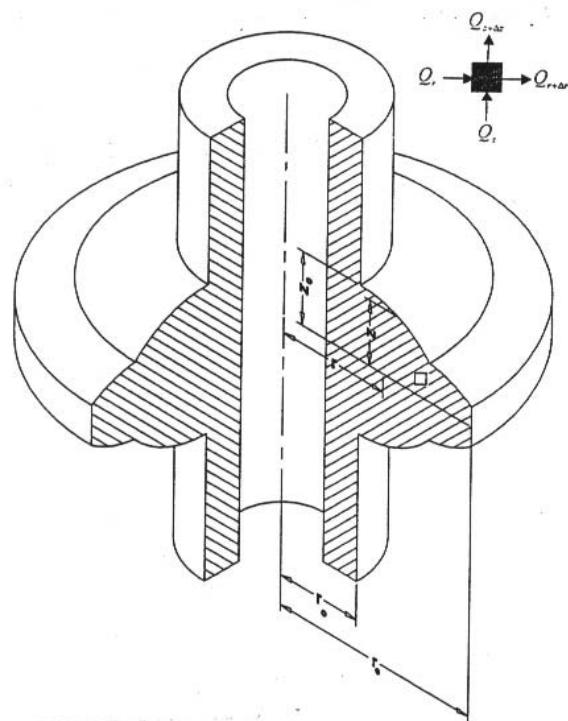
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$$(am) \quad \tilde{O} \quad \tilde{O} \quad \tilde{U} \tilde{O} \quad . \quad (7,6,5,4) \quad \tilde{U} \quad \tilde{U} \quad \tilde{U} \quad \tilde{U}$$

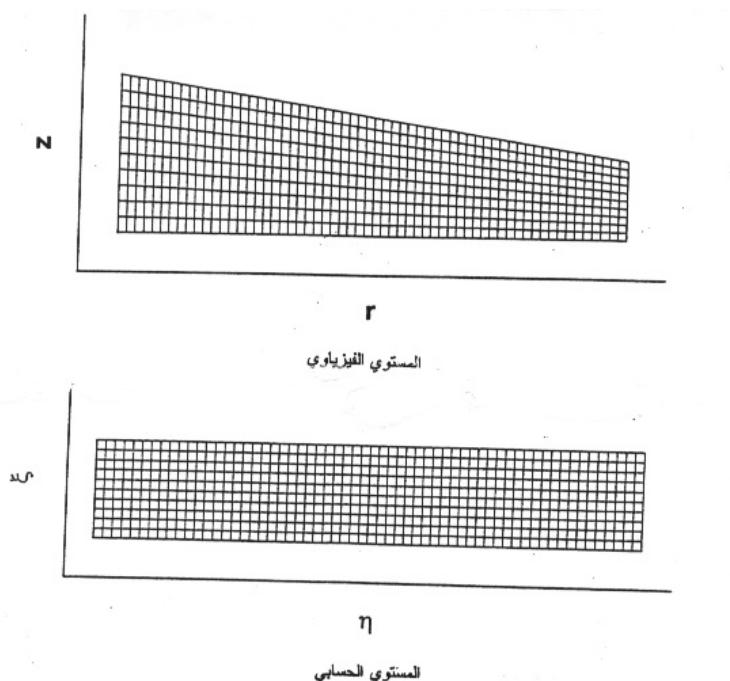
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W=0.003				
Lf	R _L	R _t	R _s	TR
0.01	56.608	1.2565	636.638	693.261
0.02	96.772	0.52355	265.266	362.040
0.03	127.926	0.29917	151.580	279.507
0.04	153.381	0.1963	99.474	252.856
0.05	174.902	0.1396	70.737	245.640
0.06	193.545	0.10471	53.0532	246.599
0.07	209.989	0.08159	41.340	251.330
0.08	224.699	0.06544	33.1582	257.857
W=0.004				
0.01	42.456	1.6753	636.638	679.127
0.02	72.579	0.6980	265.266	337.849
0.03	95.945	0.3988	151.580	247.528
0.04	115.036	0.2617	99.474	214.511
0.05	131.177	0.1861	70.737	201.914
0.06	145.159	0.1396	53.0532	198.212
0.07	157.492	0.1087	41.340	198.832
0.08	168.524	0.0872	33.1582	201.683
W=0.005				
0.01	33.965	2.0942	636.638	670.668
0.02	58.063	0.87258	265.266	323.336
0.03	76.756	0.4986	151.580	228.338
0.04	92.028	0.3272	99.474	191.504
0.05	104.941	0.2326	70.737	175.679
0.06	116.127	0.1745	53.0532	169.180
0.07	125.993	0.1359	41.340	167.334
0.08	134.819	0.1090	33.1582	157.978

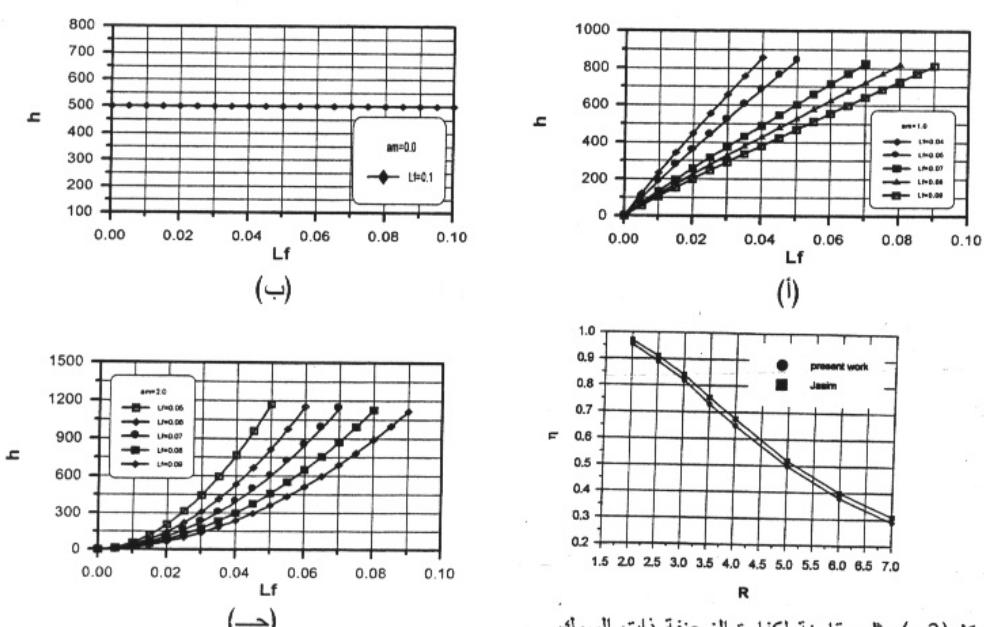
الجدول رقم(1) يمثل قيم المقاومات لزعنفة حلقيه ذات مقطع ثابت



الشكل رقم(1) يمثل مقطع عام لزعنفة حلقيه



الشكل رقم(2) يوضح تكوين الشبكة للزعنفة ذات الشكل شبه المنحرف



الشكل (3 د) يمثل مقارنة لكتافة الزعنفة ذات السمك الثابت بين العمل الحالي وعمل سابق(18)
الشكل (3، أ، ب، ج) يوضح حالات التغير لمعامل انتقال الحرارة على سطح الزعنفة

