

2004-
 (Vibration Analyzer B & K type 2515)
 Effect of Depth and Location of Circumferential Cracks on Natural Frequencies of Rotating Shaft
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 Abstract
 In this paper, An-Non destructive test procedure was used to study the effect of depth and Location of circumferential cracks on the vibration characteristics of the rotating shafts. The first procedure was to measure the natural frequencies of rotating shaft before renewing circumferential cracks with different dimensions and depths from the bearing of the rotating shaft using (vibration analyzer B & K type 2515) apparatus to analyze the vibrational characteristics during the rotation and comparing it with mathematical analysis using the method of mounting the rotating shaft. Secondly, a crack of certain depth and dimension away from the rotating shaft bearing was made. The measurements of the natural free vibration due to the presence of the crack were carried out. The study took into consideration the diameter and the length of the rotating shaft, beside the measurement of the natural free vibration of the shaft. The practical results showed a decrease in the natural frequencies of rotating shaft when the crack prested. This decrease was more when the crack located in areas near the bearing than was located away from the bearing.
 Key Word : Shaft, Crack, Circumferential, Frequency, Depth.

		ω_o
		ω
$^3 /$		ρ
-	\ddot{U}	λ_n
-		V
2		A
		A
		D
$^2 /$	\ddot{U}	E
4		I
-	\ddot{U}	K_t
-	\ddot{U}	Kts , KtL
	\ddot{U}	L
.		M
	\ddot{U}	R₁, R₂
.		T
		t
		X
-		2a/D
-	\ddot{U}	x/L

.1

\ddot{O} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U}
 [1]. \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U}
 (Unstable) \ddot{O}
 \ddot{O} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U}
 [2] \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U}
 \ddot{O} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U}
 \ddot{O} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U}
 [4] \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U}
 \ddot{O} \ddot{U} \ddot{O} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U}
 [5] (Adams)
 \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U} \ddot{U}

$\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ [6] (Dimarogonas and Massouos)
(Torsion)
 $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$
(Multi- Shaft and Multi- bearing) [4] (Davis and Mayes)
 $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$

$\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ [7] (Rajab and Al-Sabeeh)
()
 $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$

$\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ [8] (Papadopoulos)
 $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$

$\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ [3] (Behera and Parhi)
(Viscous Mediam)
 $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$

$\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ (Bearings) $\tilde{\omega}$

$\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$

$$\underline{(\omega_0)} \quad \quad \quad \emptyset \quad \quad \quad .2$$

$$\quad \quad \quad \quad \quad \quad \quad \quad \quad \quad \quad 1.2$$

$\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$

500) $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ (12 10.5 8)

$\tilde{\omega}$ [9] (2-1) $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ (700 600

$\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ $\tilde{\omega}$ (Simply-supported) $\tilde{\omega}$ $\tilde{\omega}$

$$\omega_o = \frac{\lambda_n^2}{L^2} \sqrt{\frac{EI}{\rho A}} \quad \text{-----(2-1)}$$

(K_t)

Ø

2.2

$$K_t = \frac{(K_{ts} - 1)(K_{tL} - 1)}{\sqrt{(K_{ts} - 1)^2 + (K_{tL} - 1)^2}} + 1 \quad \text{-----(2-2)}$$

$$K_{ts} = 1 + 2\sqrt{\frac{a}{t}} \quad \text{-----(2-3)}$$

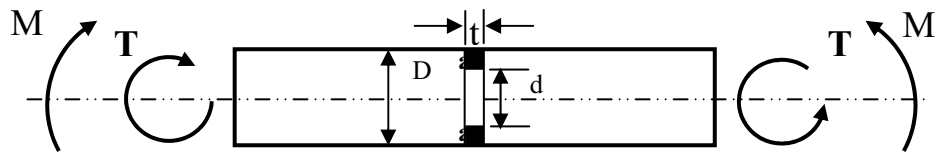
$$K_{tL} = \frac{1}{N} \frac{3}{4} \left(\sqrt{\frac{d}{2t} + 1} + 1 \right) \left(\frac{3d}{2t} - (1 - 2\nu) \sqrt{\frac{d}{2t} + 1} + 4 + \nu \right) \quad \text{-----(2-4)}$$

$$N = 3 \left(\frac{d}{2t} + 1 \right) + (1 + 4\nu) \sqrt{\frac{d}{2t} + 1} + \frac{1 + \nu}{1 + \sqrt{\frac{d}{2t} + 1}} \quad \text{-----(2-5)}$$

$$K_{ts} = 1 + \sqrt{\frac{a}{t}} \quad \text{-----(2-6)}$$

$$K_{tL} = \frac{3 \left(1 + \sqrt{\frac{d}{2t} + 1} \right)^2}{4 \left(1 + 2\sqrt{\frac{d}{2t} + 1} \right)} \quad \text{-----(2-7)}$$

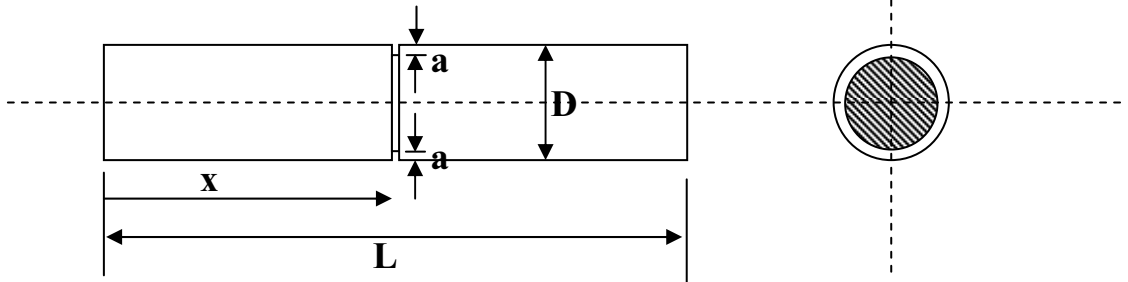
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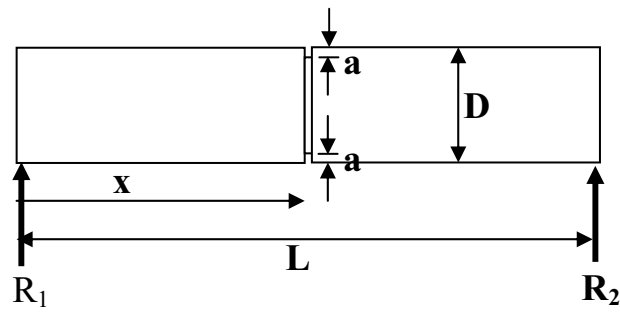
(1) Ø

3.2

\tilde{O} \tilde{O}
 \tilde{O} (D) (2a) \tilde{U} (3) \tilde{U} (2) \tilde{U} \tilde{U} (x/L)



(2) Ø



\tilde{U} (3) \tilde{U}

\tilde{U} \tilde{O} . (%0.13) (Mild Steel)

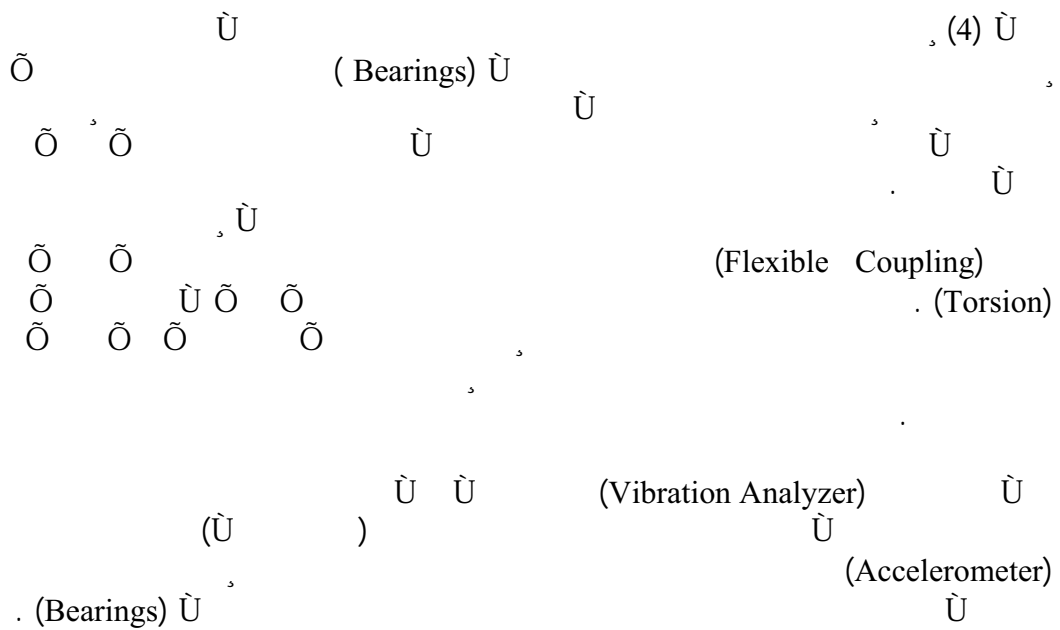
.3
1.3

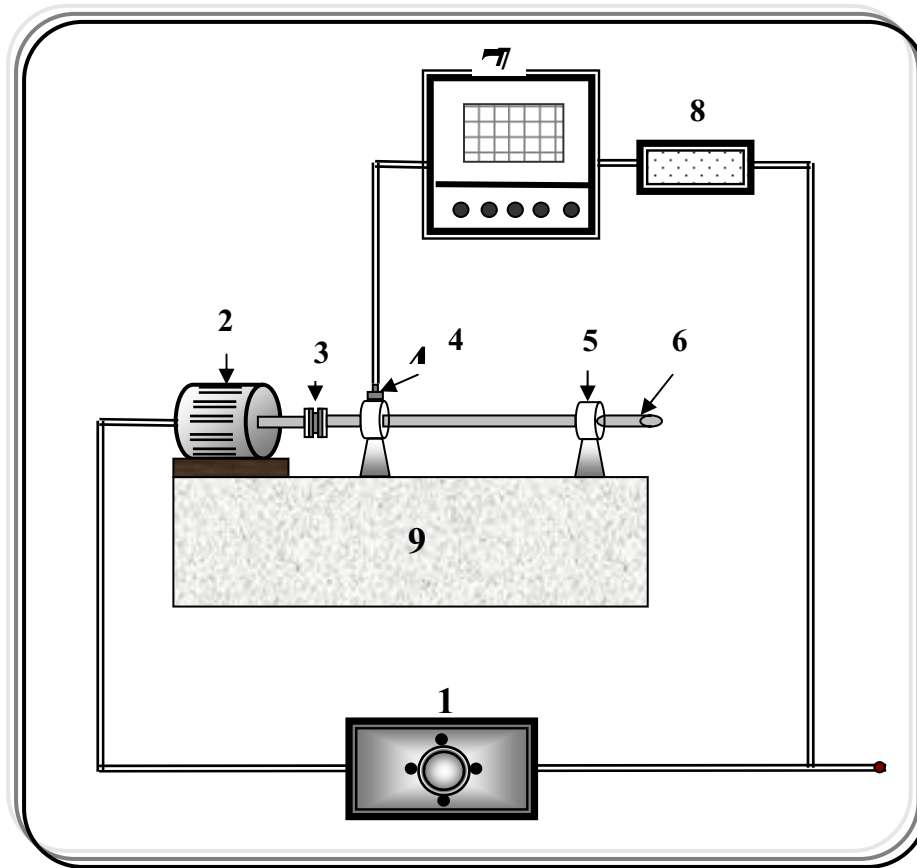
(1)

(mm)	8 , 10.5 , 12	(D)
(mm)	500 , 600 , 700	(L) Û
(Kg/m ³)	7800	(ρ)
(GN/m ²)	207	(E) Û
(MN/m ²)	280	(σ _y)
(%)	25	

(1)

2.3



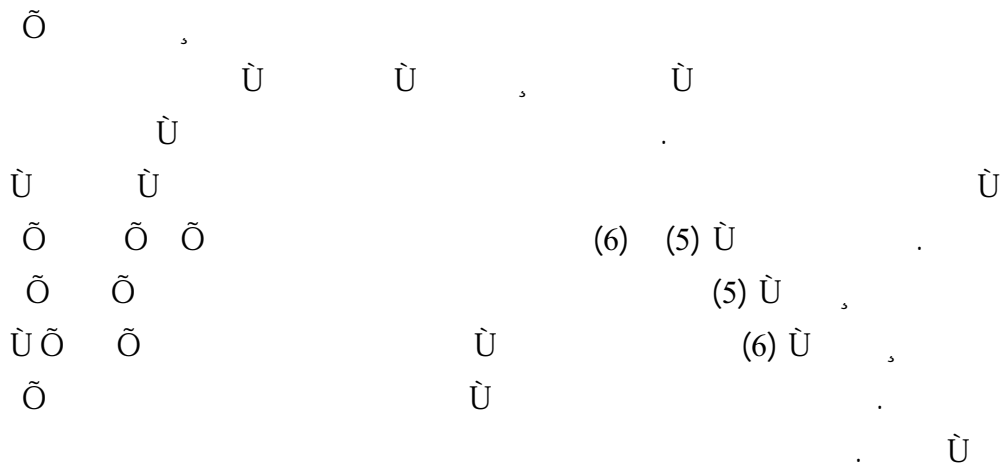


(Coupling)	-3	-2	-1
(Rotating Shaft)	-6	(Bearings)	-5
	-9	(Power Supply)	-8
			-4
			-7

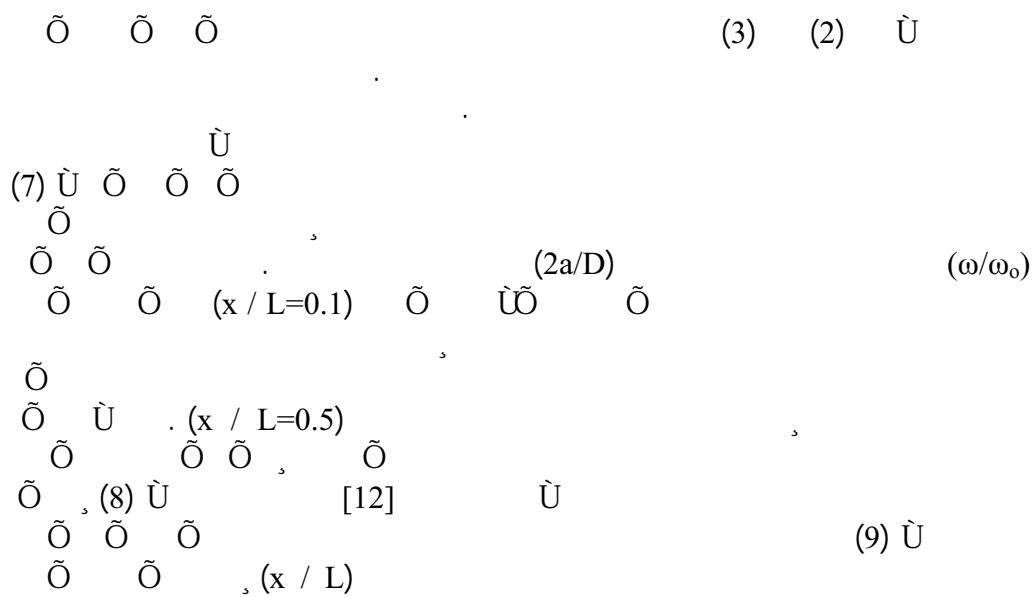
3.3

\tilde{O} \tilde{O}
 \tilde{O}
 (Vibration Analyzer B & K Type 2515)
 \tilde{O} (Spectrum) \tilde{O} \tilde{U} \tilde{U} \tilde{U}
 (Fast Fourier Transformation, (F.F.T))
 \tilde{O} \tilde{O} \tilde{O} \tilde{U}
 \tilde{U} \tilde{U} \tilde{U}
 \tilde{U} (0.5) (0.5 mm) \tilde{U}
 \tilde{U} (2a/D)

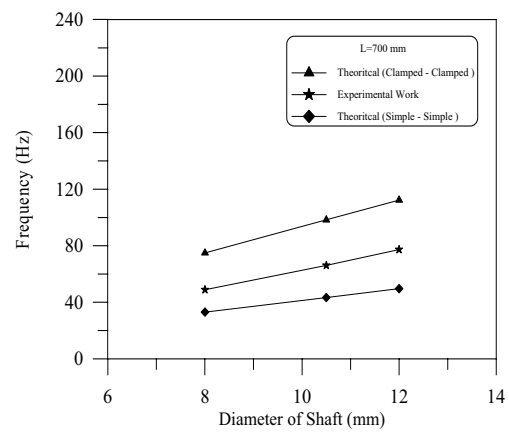
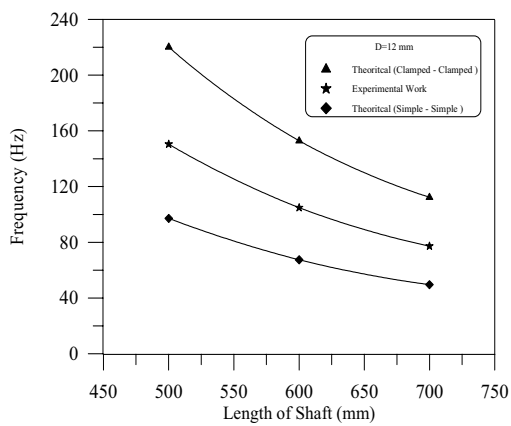
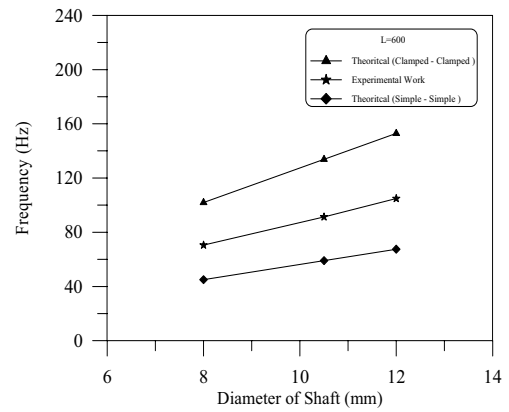
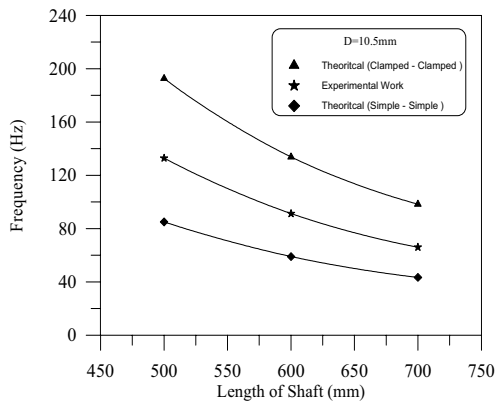
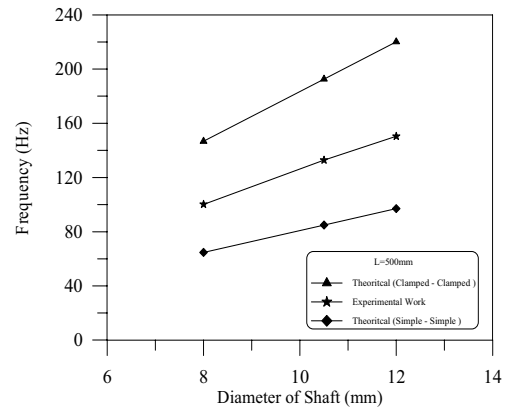
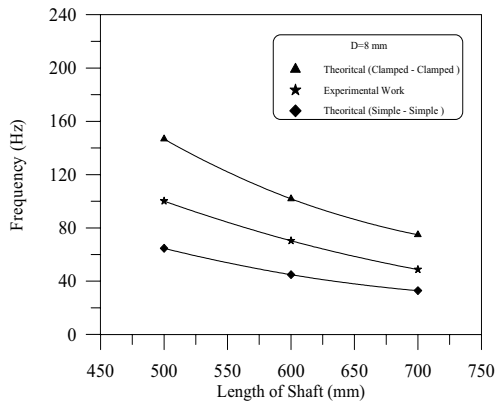
.4
1.4



2.4



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\hat{U} (6) \hat{U}

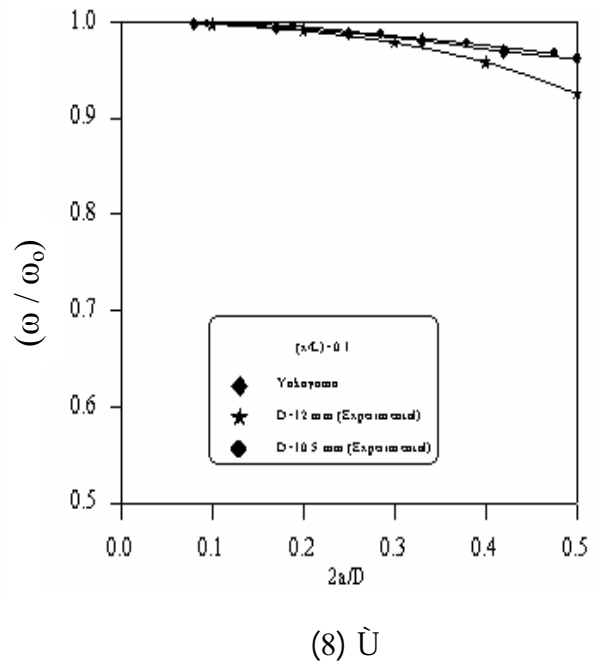
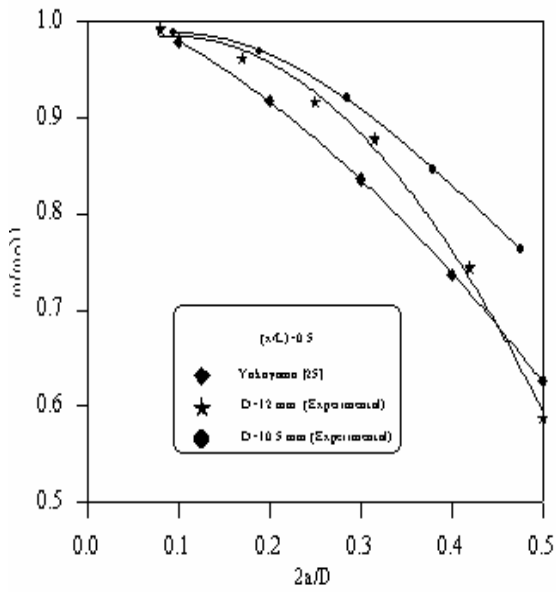
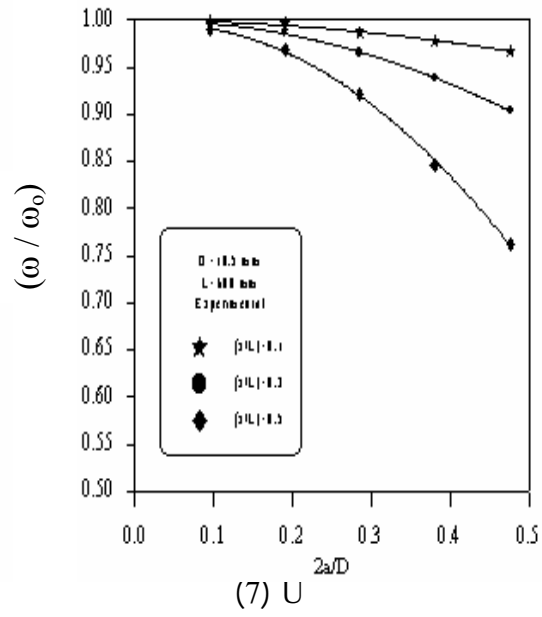
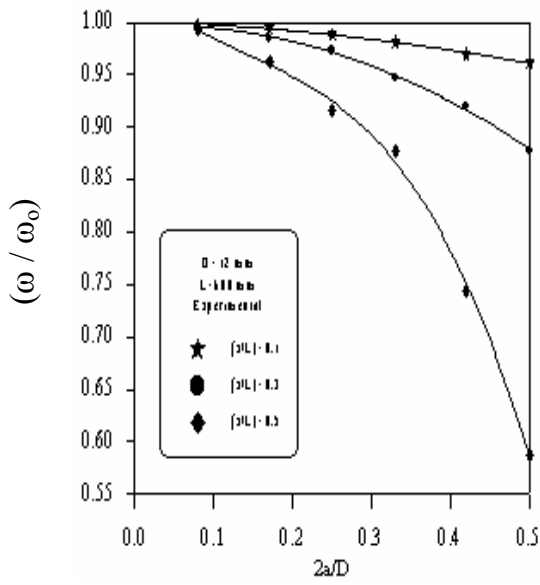
(5) \hat{U}

(x/L)			(2a/D)
(x/L)=0.5	(x/L)=0.3	(x/L)=0.1	
(ω/ω_0)			
0.9890	0.9956	0.9978	0.095
0.9692	0.9868	0.9956	0.190
0.9078	0.9649	0.9868	0.285
0.8464	0.9385	0.9780	0.380
0.7631	0.9035	0.9671	0.476

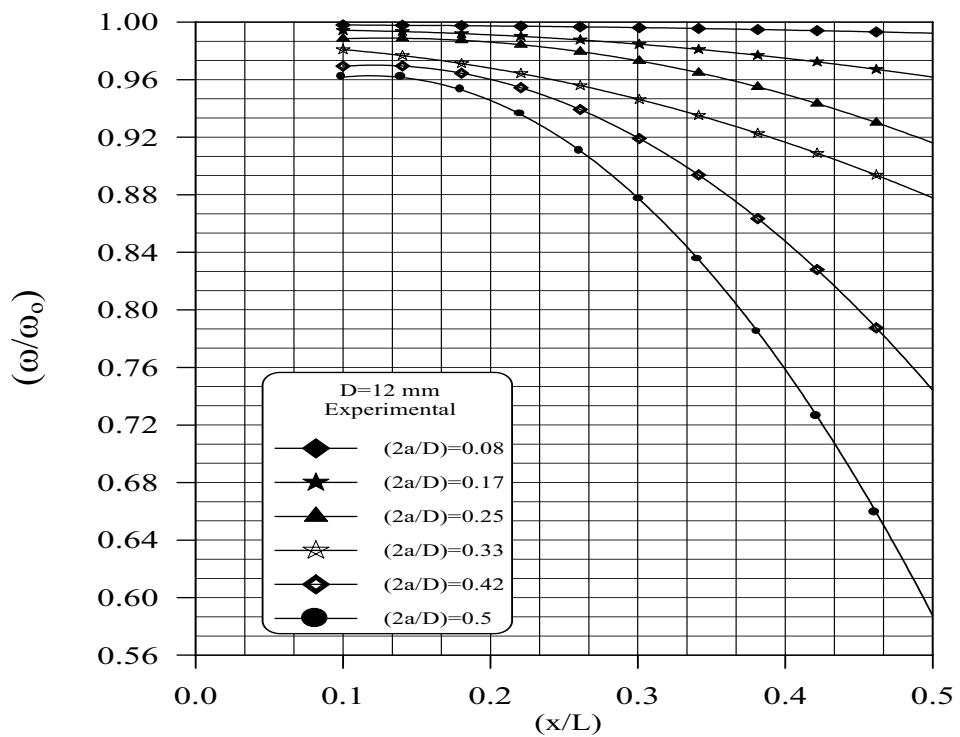
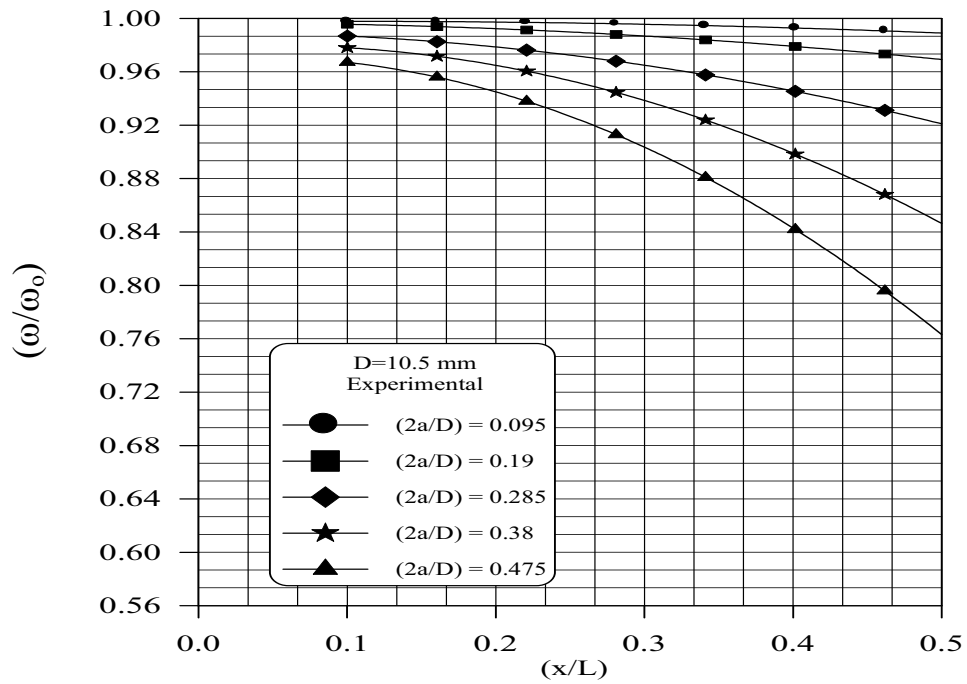
$$(10.5) \quad (600) \dot{U} \quad (2) \dot{U}$$

(x/L)			(2a/D)
(x/L)=0.5	(x/L)=0.3	(x/L)=0.1	
(ω/ω_0)			
0.9923	0.9962	0.9980	0.08
0.9618	0.9847	0.9943	0.17
0.9160	0.9732	0.9885	0.25
0.8778	0.9465	0.9809	0.33
0.7442	0.9198	0.9694	0.42
0.5877	0.8778	0.9618	0.50

$$(12) \quad (600) \dot{U} \quad (3) \dot{U}$$



[12]



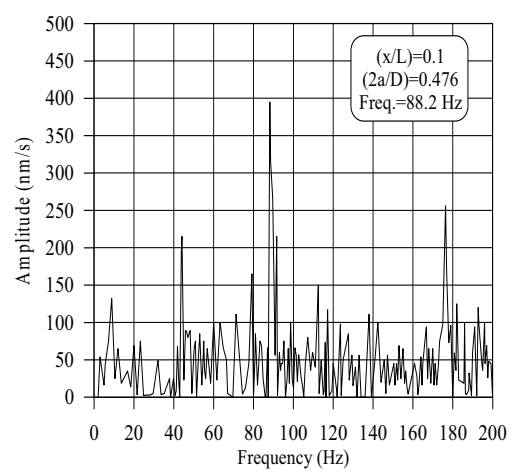
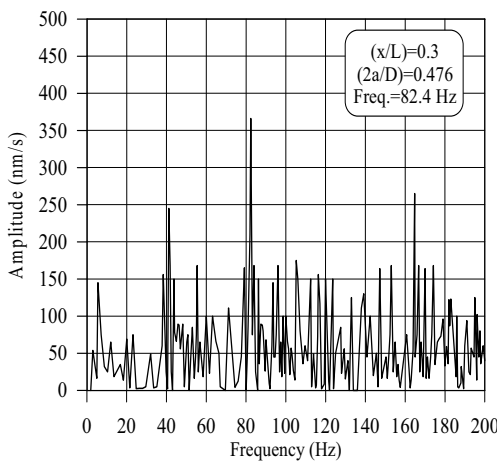
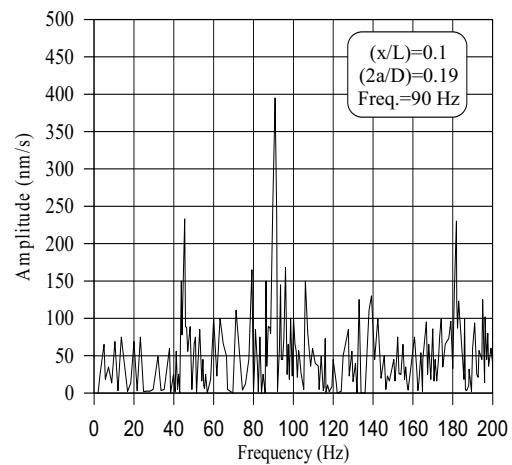
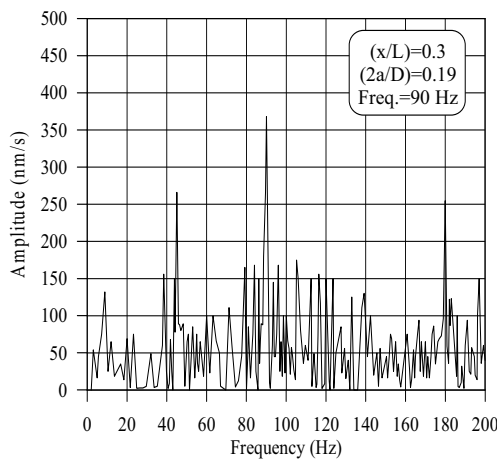
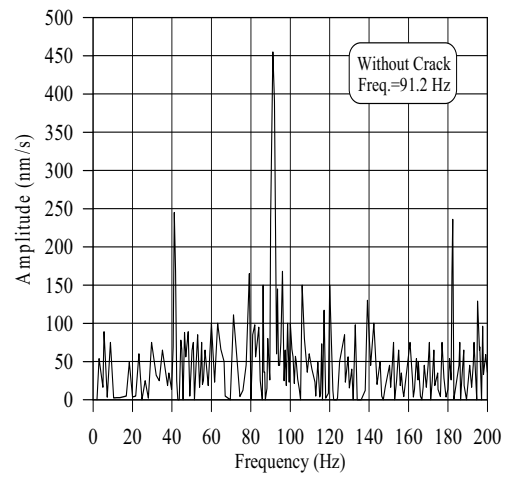
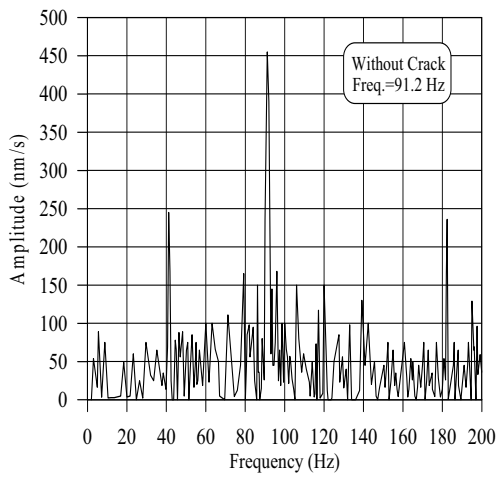
(9) \dot{U}

Ø 3.4

\tilde{U} \tilde{O} \tilde{O} \tilde{O} \tilde{O} \tilde{U}
 \tilde{O} (Amplitude) \tilde{U} (12) \tilde{U} (10) \tilde{U}
 \tilde{O} \tilde{O} (Hz) \tilde{U} (nm/sec)
 \tilde{O} \tilde{U}
 \tilde{U} \tilde{O} (10.5) \tilde{U} \tilde{U} (10) \tilde{U}
(91.2) \tilde{O} \tilde{O} \tilde{O} \tilde{U} (92.175) \tilde{U} (600)
 \tilde{O} \tilde{U} (2-1)
 \tilde{O} \tilde{O} \tilde{O} \tilde{U} (Harmonic)
 \tilde{O} \tilde{U} (Noise)
 \tilde{O} \tilde{U} \tilde{U} (x / L=0.1)
 \tilde{O} \tilde{U} \tilde{U}
 \tilde{O} \tilde{O} \tilde{O} \tilde{U} \tilde{U}
 \tilde{O} (\tilde{U}) \tilde{U}
 \tilde{O} (x / L=0.3) \tilde{O} (11) \tilde{U}
 \tilde{O} (12) \tilde{U} \tilde{O} \tilde{U}
 \tilde{O} \tilde{O} \tilde{U} ()

Ø 4.4

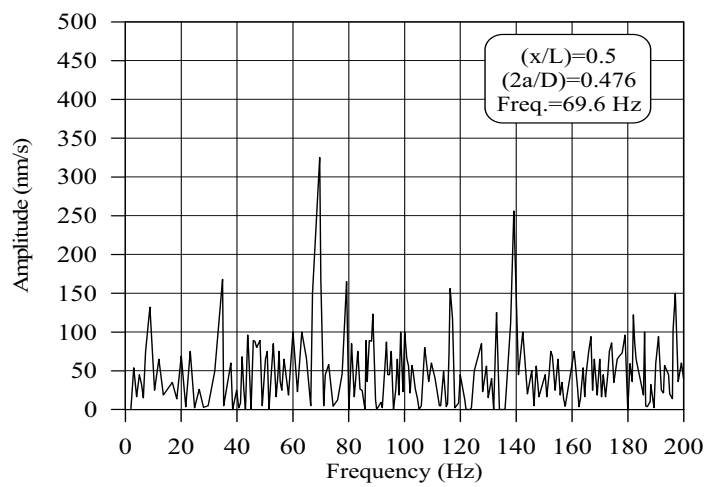
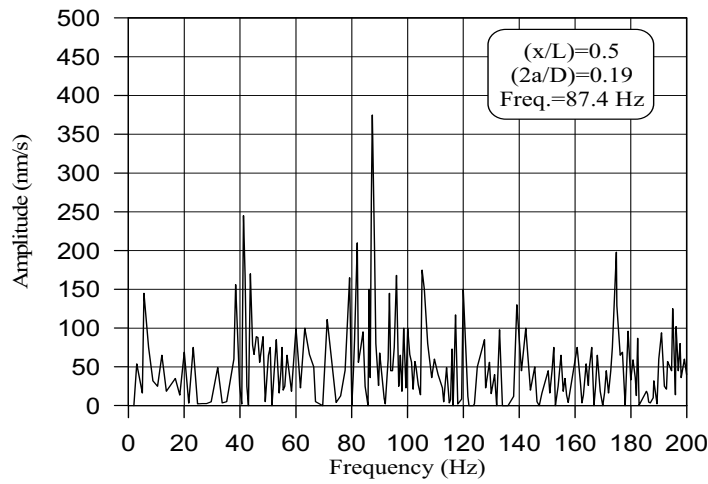
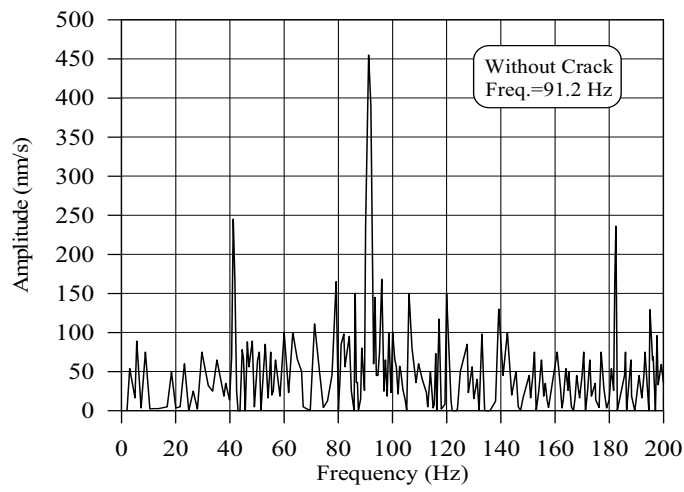
\tilde{O} \tilde{U}
 \tilde{O} (14) (13) \tilde{U}
 \tilde{O}) \tilde{U} \tilde{U}
(2a/D=0.2) \tilde{U} \tilde{U}
 \tilde{U} \tilde{O} \tilde{U} \tilde{U}
 \tilde{O} \tilde{U} \tilde{U} (2t/D)



(11) \ddot{U}

(10) \ddot{U}

:



(12) \dot{U}

$$\begin{aligned}
 & \ddot{w} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} = \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} \quad (16) \\
 & \ddot{w} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} = \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} \quad (15) \\
 & \ddot{w} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} = \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} \quad (17) \\
 & \ddot{w} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} = \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} \quad (18)
 \end{aligned}$$

[11] (Nisitani and Noda)

(V)

5

$$\begin{aligned}
 & \ddot{w} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} = \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} \quad (x/L=0.1) \\
 & \ddot{w} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} = \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} \quad (x/L=0.5) \\
 & \ddot{w} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} = \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} \quad (x/L=0.1) \\
 & \ddot{w} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} = \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} \quad (x/L=0.5)
 \end{aligned}$$

[Yokoyama and Chen]

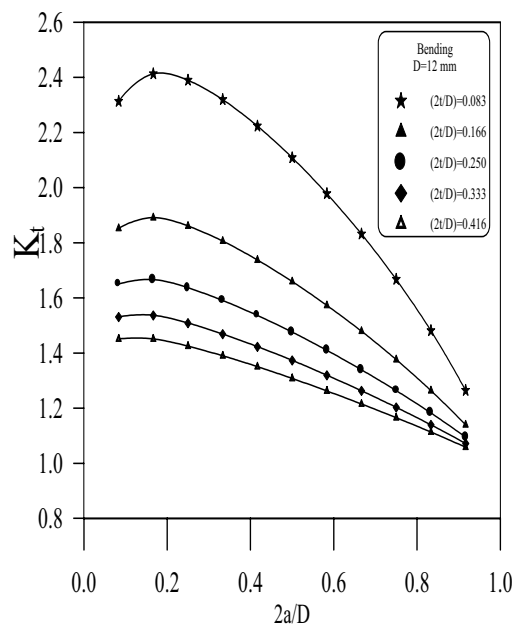
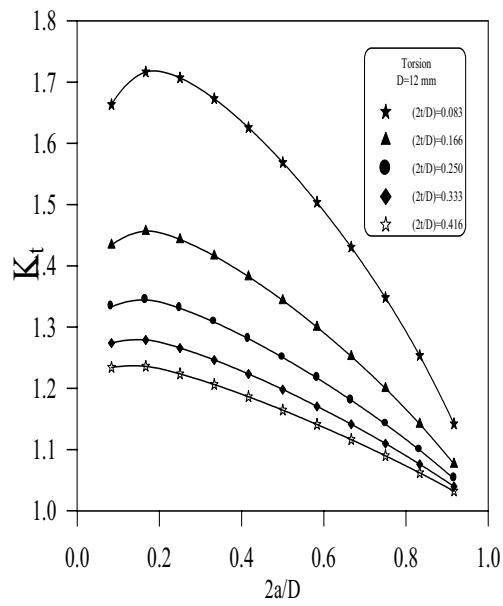
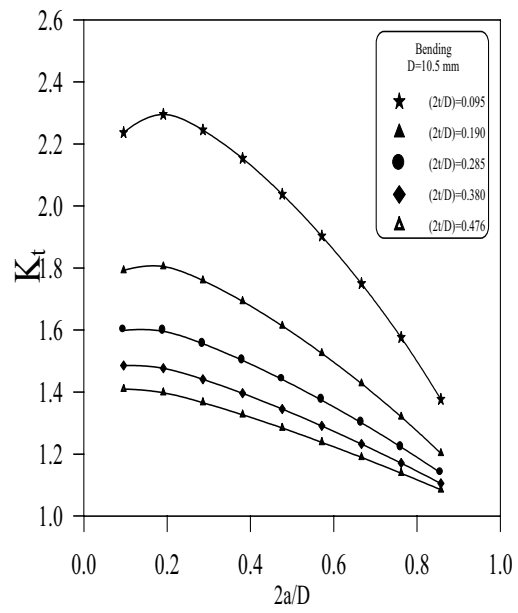
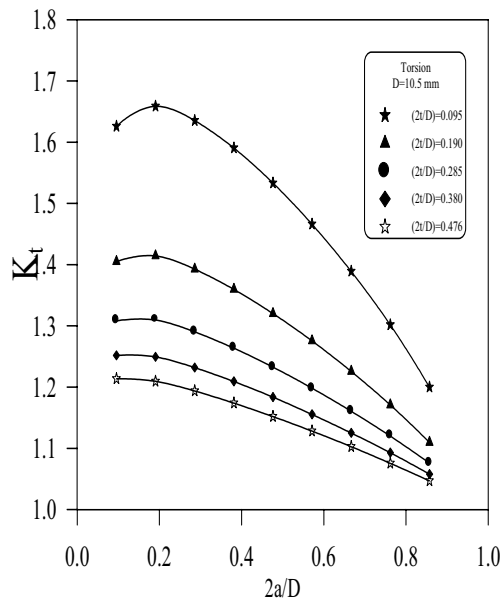
(K_t)

(2a/D)

(2t/D)

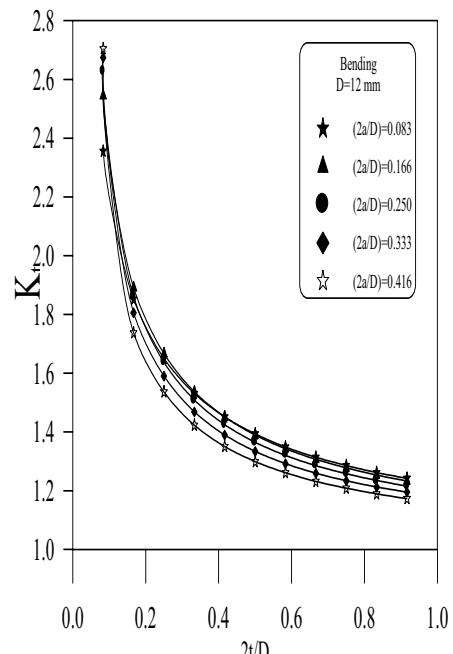
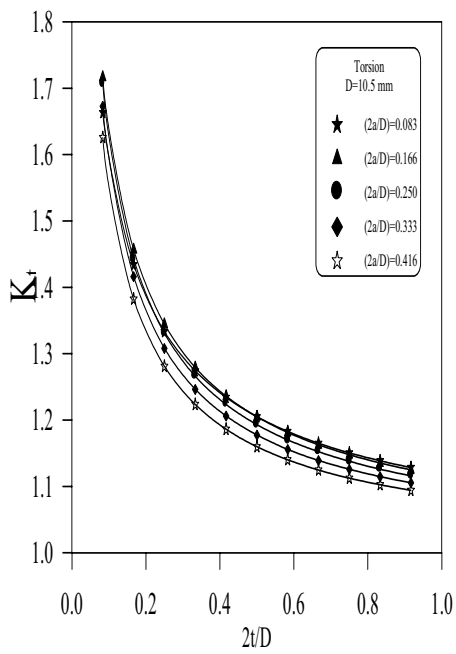
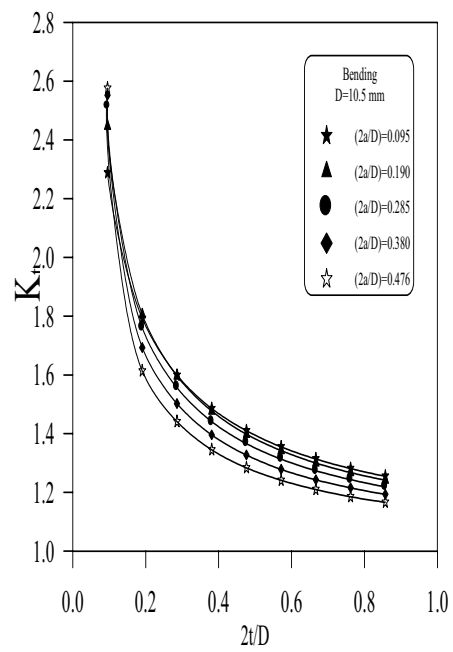
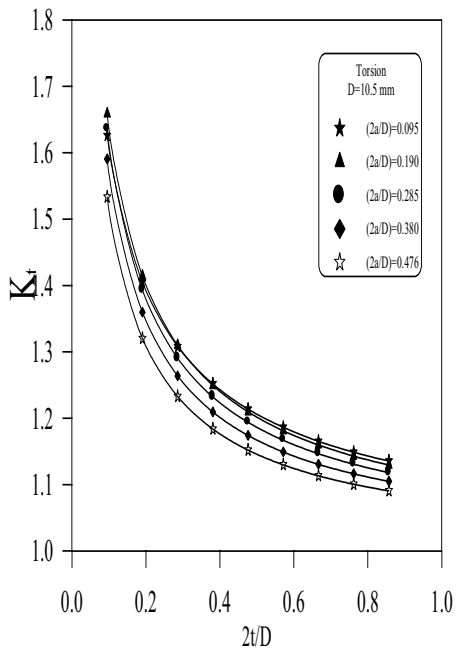
[Nisitani and Noda]

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\hat{U} (14) \hat{U}

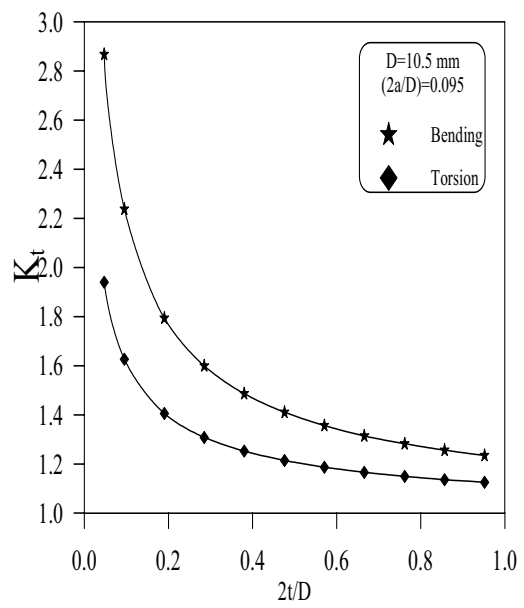
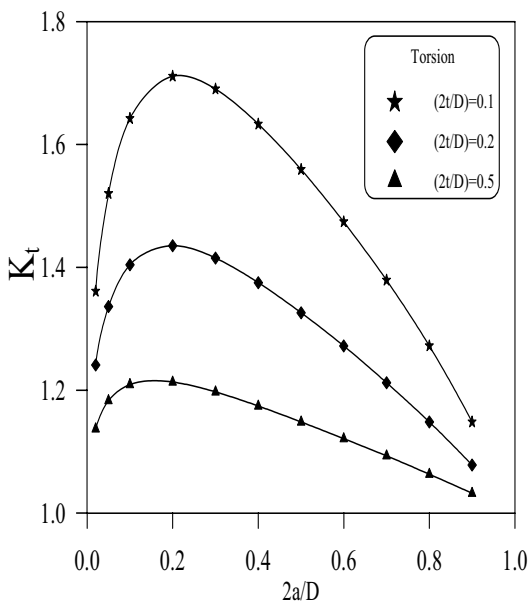
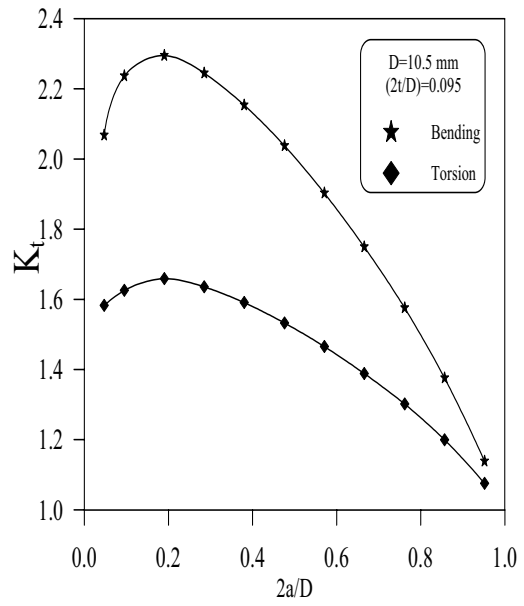
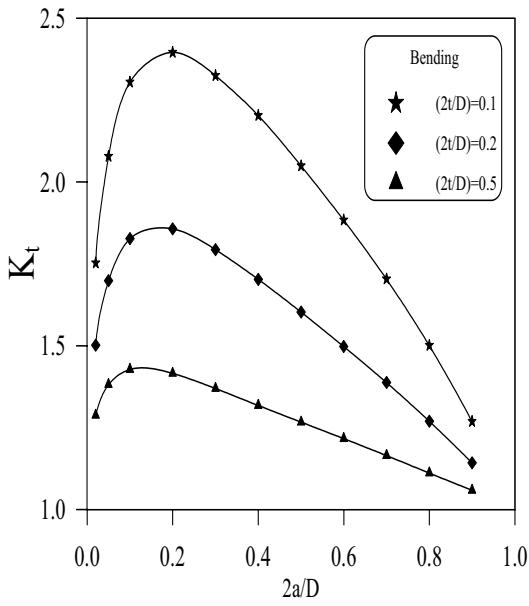
\hat{U} (13) \hat{U}



\hat{U} (16) \hat{U}

\hat{U} (15) \hat{U}

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(18) \hat{U} [11]

(17) \hat{U}

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