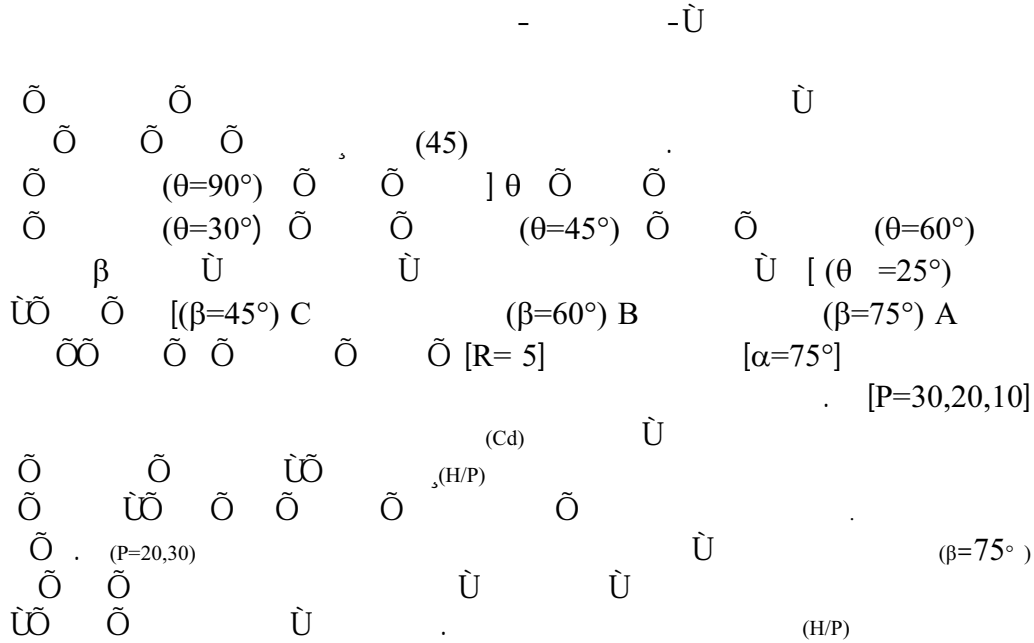


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## Coefficient of Discharge For the Normal and Oblique Weirs with Semi-Circular Crest

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### ABSTRACT

The coefficient of discharge of normal and oblique weirs with semicircular crest under free over flow conditions was studied experimentally. Forty-five weir models were constructed and tested. These models classified in to five groups based on the variation of oblique angle with the canal wall ( $\theta$ ) [group one ( $\theta=90^\circ$ ), group two ( $\theta=60^\circ$ ), group three ( $\theta=45^\circ$ ), group four ( $\theta=30^\circ$ ), group five ( $\theta=25^\circ$ )]. Each group included three series of tests depending on the variation of downstream face slope ( $\beta$ ) [series A ( $\beta=75^\circ$ ), series B ( $\beta=60^\circ$ ), series C ( $\beta=45^\circ$ )]. The upstream slop was fixed for all models with angle ( $\alpha =75^\circ$ ) and the crest radius ( $R=5$ ) cm. Every series included testing of three models based on the variation of weir height [ $P=30,20\&10$  cm].

The experimental results of the study showed that the discharge coefficient ( $C_d$ ) increases with the increase of water depth above the crest to the weir height ratio ( $H/P$ ), and with the increase of downstream slope ( $\beta$ ) the peak values of ( $C_d$ ) were found when downstream face slope ( $\beta=75^\circ$ ) and weir height ( $P=10$  cm). In case of oblique weirs, it was found that ( $C_d$ ) decreases with increase of ( $H/P$ ) values. Also it was found that ( $C_d$ ) increases with the increase of the downstream slope ( $\beta$ ) & weirs of small oblique angle ( $\theta$ ) give low values of ( $C_d$ ).

**Keywords:** Weirs; Free-fall Structures Experimental Study

- $\dot{U} = C_d$
- $\dot{U} = g$
- $\dot{U} = h$
- $\dot{U} = L$
- $\dot{U} = P$
- $\dot{U} = Q_{NC}$
- $\dot{U} = Q_{NS}$
- $\dot{U} = Q_{OB}$
- $\dot{U} = R$
- $\dot{U} = Re$
- $\dot{U} = V$
- $\dot{U} = B$
- $\dot{U} = \mu$
- $\dot{U} = \rho$
- $\dot{U} = \theta$
- $\dot{U} = \alpha$
- $\dot{U} = \beta$
- $\dot{U} = f, f_1, f_2$

(Ramamurthy and Vo,1994 )

(Ibraheem et al.,1988)

Ù ( Abid Ali,1989)

Ù ( Ramamurthy and Vo,1994)

Ù (  $\beta=45^\circ$ ) Ù (  $\alpha =90^\circ$ ) Ù -1  
Ù (Cd)

(5.5) ( H/R)  
(Cd) (H/R>3) Ù Ù -2

Ù ( Chilmerran, T. A. 1996)

Ù (Chanson and Montes,1998 )

Ù (D/R) Ù

Ù (Ziba Vatannia,1999)

Ù (H/P) Ù Ù Ù Ù

(AL-Humaidawa,2000)

Ù (  $\theta$ ) Ù (Cd) Ù

(Al-Tikrity, R., 2000 )

Ù

( Abdel-Azim M. Negm et al.,2002)

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Ù ( 45) (30) (10) Ù

Ù (  $\theta$ ) ( 45) (1) Ù

Ù (5) (  $\theta=45^\circ$ ) Ù (  $\theta=60^\circ$ ) Ù (  $\theta=90^\circ$ )

$\tilde{O}$   $\tilde{U}$   $[(\theta = 25^\circ)$   $\tilde{U}$   $(\theta = 30^\circ)$   
 $(\beta = 60^\circ) B$   $\tilde{O}$   $(\beta = 75^\circ) A$   $], (\beta)$   $\tilde{U}$   $\tilde{U}$   
 $[\alpha = 75^\circ]$   $\tilde{U}$   $\tilde{U}$   $\tilde{U}$   $[(\beta = 45^\circ) C$   $\tilde{U}$   
 $(1) \tilde{U} \tilde{O}$   $(P = 30, 20, 10)$   $\tilde{O}$   $\tilde{U}$   $[R = 5]$   
 $\tilde{U}$   $(2) \tilde{U}$

$\tilde{U}$   $(315)$   $(B.S.I 1965) \tilde{O}\tilde{O}\tilde{O}\tilde{O}$   
 $(2.5)$   $\tilde{U}$   $(7)$   
 $(White 1977) ( )$   $(40)$   
 $\tilde{U}$   $(Q_{NC})$   
 $(H)$   $(H)$   $(P)$   $(Q_{NS})$   
 $(Rehbock) \tilde{O}\tilde{O}$

$$Q_{NS} = \frac{2}{3} C_d \sqrt{2g} L H_e^{1.5} \dots\dots\dots(1)$$

$$C_d = (0.602 + 0.083 \frac{H}{P})$$

$$H_e = (H + 0.0012)$$

$( / )$   $= Q_{NS} = P$   
 $( )$   $\tilde{U}$   
 $-:$

$$C_d = \frac{Q_{NC}}{\frac{2}{3} \sqrt{2g} L H^{1.5}} \dots\dots\dots(2)$$

$( / )$   $= Q_{NC}$   
 $\emptyset$

$\tilde{U}$   
 $-:$

$$f(q, H, P, g, \rho, \mu, \beta, \theta) = 0 \dots\dots\dots(3)$$

$(L^3/T.L)$   $\tilde{O}$   $\tilde{U}$   $= q$   
 $(L)$   $= H$   
 $(L/T^2)$   $\tilde{O}$   $\tilde{O}$   $\tilde{O}$   $= P$   
 $\tilde{U}$   $= (L) g$



(Ramamurthy & Vo, 1994)<sup>1</sup> (Escande & Sananes, 1959)  
 (p=10) (β=75°) (2) (θ)  
 (C<sub>d</sub>) (H/P) (H/P)  
 (Q<sub>OB</sub>) (Ibraheem, 1983) (Noori & Hayawi, 1999); (Noori & Hayawi, 1996); (Chilmeran, 1996)  
 (0.852) (0.567) (θ=60°, β=75°, P=30) (θ=25°, β=75°, P=30)  
 (H/P=0.14) (AL-Humaidawa, 2000; AL-Qasser, 1983)

$$C_d = \frac{Q}{A \sqrt{2gH}} \quad (6)$$

(SPSS Ver.10)  
 (C<sub>d</sub>) (C<sub>d</sub>) (10) (0.926)

$$C_d = 0.7883 * \left[ \left( \frac{H}{P} \right)^{0.01748} * (\sin \theta)^{0.5131} * (\beta)^{0.3127} \right] \quad \dots\dots\dots(6)$$

(Degrees) = θ  
 (Radian) = β  
 (C<sub>d</sub>) (C<sub>d</sub>) (10) (0.926)

$$C_d = \frac{Q}{A \sqrt{2gH}} \quad (10)$$

(Chilmeran, 1996)  
 (θ=60°) (R=5) (P=30,20) (β=90°) (β=75°)

$\bar{U}$       $\bar{U}$           $\bar{U}$       $\bar{U}$      (3)  $\bar{U}$   
 $\bar{U}$          (P)      $\bar{U}$       $\bar{U}$      (H/P)  
 $\bar{U}$      (H/P)      $\bar{U}$       $\bar{U}$      ( $\theta=60^\circ$ )  
 $\bar{U}$       $\bar{U}$           $\bar{U}$      , (P)  
 $\bar{U}$           $\bar{U}$      .  
Escande & )      $\bar{U}$       $\bar{U}$       $\bar{U}$       $\bar{U}$       $\bar{U}$       $\bar{U}$           $\bar{U}$       $\bar{U}$       $\bar{U}$       $\bar{U}$       $\bar{U}$   
(H/P)  
(Ramamurthy & Vo, 1994);(Sananes, 1959  
 $\bar{U}$   
 $\bar{U}$   
 $\bar{U}$      (C<sub>d</sub>)      $\bar{U}$       $\bar{U}$       $\bar{U}$       $\bar{U}$      (C<sub>d</sub>)      $\bar{U}$      -1  
 $\bar{U}$      (H/P)  
(P)  
(P=10)     ( $\beta=75^\circ$ )      $\bar{U}$      -2  
 $\bar{U}$      (C<sub>d</sub>)      $\bar{U}$      ( $\beta$ )      $\bar{U}$      -3  
 $\bar{U}$       $\bar{U}$       $\bar{U}$       $\bar{U}$      -4  
 $\bar{U}$       $\bar{U}$       $\bar{U}$       $\bar{U}$       $\bar{U}$      ( $\theta=25^\circ$ )  
 $\bar{U}$       $\bar{U}$       $\bar{U}$       $\bar{U}$       $\bar{U}$      ( $\theta=60^\circ, 45^\circ, 30^\circ$ )

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∅ : (1)∅

Crest Height P(cm)	Crest Length L (cm)	Downstream angle (β)	Upstream angle (α)	Series No.	Crest Radius R (cm)	Oblique angle (θ)	Model No.	group No.
30, 20, 10	30	75°	75°	A	5	90° (Normal weir)	1 - 3	1
30, 20, 10	30	60°		B			4 - 6	
30, 20, 10	30	45°		C			7 - 9	
30, 20, 10	34.6	75°	75°	A	5	60°	10 - 12	2
30, 20, 10	34.6	60°		B			13 - 15	
30, 20, 10	34.6	45°		C			16 - 18	
30, 20, 10	42.424	75°	75°	A	5	45°	19 - 21	3
30, 20, 10	42.424	60°		B			22 - 24	
30, 20, 10	42.424	45°		C			23 - 27	
30, 20, 10	60	75°	75°	A	5	30°	28 - 30	4
30, 20, 10	60	60°		B			31 - 33	
30, 20, 10	60	45°		C			34 - 36	
30, 20, 10	70.98	75°	75°	A	5	25°	37 - 39	5
30, 20, 10	70.98	60°		B			40 - 42	
30, 20, 10	70.98	45°		C			43 - 45	

∅ : (2)∅

∅									(θ°)	P (cm)
β=45°			β=60°			β=75°				
Min.	Max.	H/P	Min.	Max.	H/P	Min.	Max.	H/P		
0.750	0.821	0.860	0.777	0.856	0.835	0.838	0.899	0.810	°90	10
0.643	0.743	0.530	0.687	0.818	0.480	0.750	0.931	0.402	60°	
0.586	0.675	0.440	0.635	0.743	0.400	0.692	0.847	0.320	°45	
0.466	0.553	0.405	0.514	0.649	0.300	0.584	0.671	0.340	°30	
0.453	0.567	0.300	0.473	0.586	0.300	0.516	0.632	0.310	°25	
0.711	0.758	0.400	0.747	0.809	0.404	0.790	0.850	0.395	°90	20
0.599	0.711	0.265	0.639	0.782	0.230	0.709	0.871	0.210	60°	
0.554	0.651	0.210	0.602	0.704	0.218	0.649	0.795	0.215	°45	
0.438	0.522	0.205	0.485	0.617	0.155	0.556	0.649	0.150	30°	
0.424	0.530	0.150	0.447	0.558	0.155	0.486	0.584	0.170	25°	
0.664	0.743	0.233	0.709	0.790	0.240	0.73	0.825	0.237	90°	30
0.586	0.693	0.160	0.619	0.759	0.155	0.675	0.852	0.137	60°	
0.531	0.636	0.145	0.588	0.689	0.145	0.637	0.785	0.103	45°	
0.427	0.507	0.143	0.474	0.600	0.123	0.536	0.639	0.103	30°	
0.412	0.498	0.107	0.429	0.548	0.100	0.475	0.567	0.127	25°	

∅ : (3)∅

(2-1)	(2)	(1)	H/P	p(cm)	(θ)
	(β=90°)	(β=75°)			
Δ Cd (%)	∅ (Cd) ∅	(Cd) ∅			
-24.11	0.591	0.7335	0.14	30	90°
-7.63	0.695	0.748	0.16		
-27.71	0.599	0.765	0.18		
-29.00	0.607	0.783	0.2		
-30.47	0.617	0.805	0.22		
-35.04	0.585	0.790	0.28	20	
-36.22	0.588	0.801	0.3		
-37.16	0.592	0.812	0.32		
-38.32	0.595	0.823	0.34		
-39.30	0.598	0.833	0.36		
-19.01	0.710	0.845	0.14	30	60°
-11.42	0.718	0.800	0.16		
-6.59	0.713	0.760	0.18		
-1.41	0.71	0.720	0.2		
0.00	0.706	0.706	0.22		
-24.66	0.734	0.915	0.18	20	
-20.90	0.732	0.885	0.20		
-17.65	0.731	0.860	0.22		
-14.35	0.7311	0.836	0.24		
-10.58	0.7325	0.810	0.26		

