

$$\begin{aligned}
 & \frac{1}{\bar{E}_p} = \frac{1}{\bar{E}_p} + \frac{1}{\bar{E}_p} \quad (20) \\
 & \frac{1}{\bar{E}_p} = \frac{1}{\bar{E}_p} + \frac{1}{\bar{E}_p} \quad (20) \\
 & \text{Doorenbos } \bar{E}_p \quad [1] \\
 & \bar{E}_p \quad \bar{E}_p \quad [2] \text{ (Al-Kassam 1979)} \\
 & \text{(FAO)}
 \end{aligned}$$

Predicting Yield Response Factors In Jensen Model

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Abstract

The yield response model is very important in irrigation planning and management of irrigation projects. A computerized model for simulating irrigation water requirement for wheat crop at Mosul area has been proposed for (20)years of daily climatological data. The model predict daily actual and potential evapotranspiration, then the relation between relative yield and relative evapotranspiration is put into (20)equations and solved mathematically to find the coefficients for each stage of growing growth period of wheat crop at Mosul area. The yield response factors is found for two cases, the first is for rainfed agriculture practice for wheat for (20)years where an available data for production is available ,and the second is for irrigated practice where four years production data were available[1] .Then the results are compared with the results obtained from (Doorenbos & Al kassam 1979) equation for yield. [2] and show a small variation while the last equation is justified by International Agriculture and Food Organization(FAO).

Keywords: crop water production function ,yield response factor, yield Jensen model, irrigation management.

\tilde{O} \tilde{O} \tilde{O} \tilde{O} \tilde{U} \tilde{U}
 \tilde{O} -
 \tilde{O} \tilde{O}
 \tilde{O} \tilde{O} \tilde{O} \tilde{U} [3,4,5] -

:Hanks

$$Y/Y_{\max} = T/T_{\max} \dots\dots\dots(1)$$

:
 Y
 : Y_{max}
 : T
 : T_{max}

[2,6,7] -

$$Y/Y_{\max} = \prod_{i=1}^n (AET_i / CPET_i)^{\lambda_i} \dots\dots\dots(2)$$

:
 - = AET_i
 \tilde{U} - = CPET_i
 $\tilde{U} = \lambda_i$
 $\tilde{U} = n$

\tilde{O} \tilde{U} \tilde{U} λ_i \tilde{U}
 Doorenbos) \tilde{U} \tilde{U} \tilde{U} \tilde{U} \tilde{U} λ_i
 : [2] (and Al-Kassam 1979)

$$Y/Y_{\max} = \prod_{i=1}^n [1 - k y_i (1 - AET_i / CPET_i)] \dots\dots\dots(3)$$

:

$\lambda = 0.275 ky^3 - 0.1351 ky^2 + 0.8761 ky - 0.0187$ (4)

[8] (Kipkorir2002)

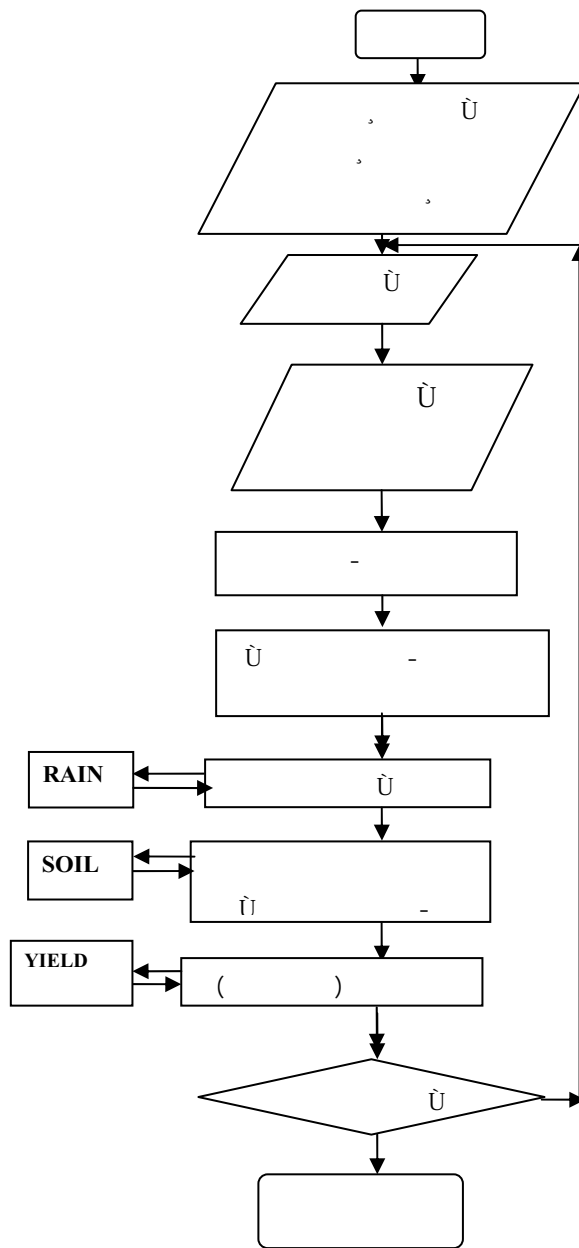
$$\lambda = 0.275 ky^3 - 0.1351 ky^2 + 0.8761 ky - 0.0187 \dots\dots(4)$$

$\lambda = 0.275 ky^3 - 0.1351 ky^2 + 0.8761 ky - 0.0187$ (4)

[9,10]

$$ET_o = \frac{0.408\Delta(R_n - G) + \gamma \frac{900}{T + 273} U_2 (es - ea)}{\Delta + \gamma(1 + 0.34U_2)} \dots\dots(5)$$

- mm/day : ET_o
- $^{\circ}c$: T
- m/sec : U_2
- $MJ/m^2 \text{ day}$: R_n
- $MJ/m^2 \text{ day}$: G
- KPa : es
- KPa : ea
- KPa : $es - ea$
- KPa / c° : Δ
- KPa / c° : γ



(1) Û

:

CPET=Kc*Eto.....(6)

mm U - =CPET = Kc

:[11]

AET=CPET* SK(7)

mm - =AET = SK

:[11] U

SK=log(1+PAW)/log 101(8)

% U :SK =PAW

: PAW

PAW=(AW/TAW)*100.....(9)

mm U :AW mm U :TAW

: TAW TAW=RZ*(FC-PWP).....(10)

cm :RZ mm/cm :FC mm/cm U :PWP

$$P_{\text{irr}} = \frac{P_{\text{irr}}}{P_{\text{irr}}} - \frac{P_{\text{irr}}}{P_{\text{irr}}} \quad [11] (10\text{mm})$$

$$AW_i + IRR + RAIN = AET + DRAIN + AWe \dots\dots\dots(11)$$

mm = AW_i
 mm = AWe
 mm = IRR
 mm = RAIN
 mm = DRAIN

20) (31) (75) (20) (35) (20) (1998-1995)

/		
U		(1) U
2930	2760	95/11/29
4081	4046	96/1/2
3952	3872	96/2/7
5500	4710	96/12/1
5470	4560	97/1/5
3490	3130	97/2/1
4610	2160	97/12/30
1090	460	97/2/17

$$\begin{aligned}
 & \tilde{O}_1 \tilde{O}_2 \tilde{O}_3 \tilde{O}_4 \tilde{O}_5 \quad (12) \\
 & \tilde{O}_1 \tilde{O}_2 \tilde{O}_3 \tilde{O}_4 \tilde{O}_5 \quad (20) \quad (12) \\
 & 0.90 = (0.75)^{\lambda_1} (0.91)^{\lambda_2} (0.96)^{\lambda_3} (0.89)^{\lambda_4} (0.91)^{\lambda_5} \\
 & 0.99 = (0.55)^{\lambda_1} (0.90)^{\lambda_2} (0.96)^{\lambda_3} (0.91)^{\lambda_4} (0.97)^{\lambda_5} \\
 & 1.00 = (0.55)^{\lambda_1} (0.90)^{\lambda_2} (0.96)^{\lambda_3} (0.89)^{\lambda_4} (0.91)^{\lambda_5} \\
 & 0.97 = (0.86)^{\lambda_1} (0.90)^{\lambda_2} (0.47)^{\lambda_3} (0.65)^{\lambda_4} (0.89)^{\lambda_5} \dots\dots\dots(12) \\
 & 0.95 = (0.86)^{\lambda_1} (0.90)^{\lambda_2} (0.47)^{\lambda_3} (0.80)^{\lambda_4} (0.90)^{\lambda_5} \\
 & \cdot \\
 & \cdot \\
 & \cdot \\
 & \cdot \\
 & \cdot \\
 & 0.97 = (0.90)^{\lambda_1} (0.90)^{\lambda_2} (0.47)^{\lambda_3} (0.66)^{\lambda_4} (0.25)^{\lambda_5}
 \end{aligned}$$

$$\begin{aligned}
 & \tilde{O}_1 \tilde{O}_2 \tilde{O}_3 \tilde{O}_4 \tilde{O}_5 \\
 & \tilde{O}_1 \tilde{O}_2 \tilde{O}_3 \tilde{O}_4 \tilde{O}_5 \quad \lambda_5, \lambda_4, \lambda_3, \lambda_2, \lambda_1 \\
 & \quad \quad \quad Y_{max} \quad \tilde{O}_1 \\
 & \quad \quad \quad \cdot [12] \\
 & \tilde{O}_1 \tilde{O}_2 \quad -2-\tilde{O}_1
 \end{aligned}$$

λ_1	λ_2	λ_3	λ_4	λ_5
0.76	3.14	0.32	3.84	2.74

\tilde{O} -3- \hat{U}

\hat{U}

$\lambda 1$	$\lambda 2$	$\lambda 3$	$\lambda 4$	$\lambda 5$
0.41	3.07	0.01	-4.58	3.41

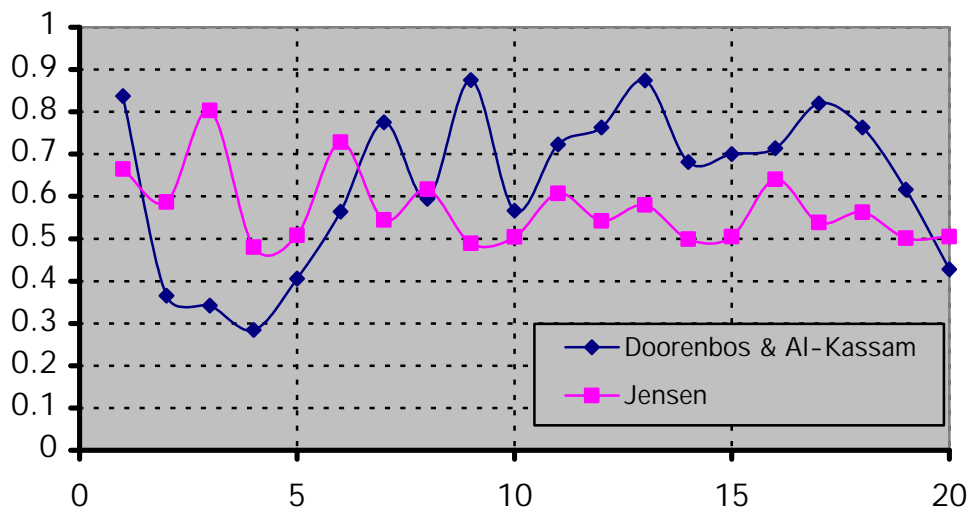
\tilde{O} Y_{max} \tilde{O} (4) \hat{U}

-4- \hat{U}

$\lambda 1$	$\lambda 2$	$\lambda 3$	$\lambda 4$	$\lambda 5$
0.54	-20.2	8.0	2.98	0.37

(2) λ_i

(2) \hat{U} (3) \hat{U}



(2) \hat{U}

$$\begin{aligned}
 & \tilde{U} \tilde{O} \quad \tilde{O} \quad \tilde{O} \quad \tilde{U} \quad \tilde{U} \quad \lambda_i \\
 & \tilde{O} \quad \tilde{O} \quad \tilde{O} \quad \tilde{O} \quad (1)\tilde{U} \quad \lambda_i \\
 & (3) \quad \tilde{O} \quad \tilde{O} \quad \tilde{O} \quad \tilde{O} \quad \tilde{U} \quad (12) \quad \tilde{U} \quad (3) \\
 & \quad \tilde{O} \quad \tilde{O} \quad \tilde{O} \quad \tilde{O} \quad \tilde{U} \quad (\quad) \quad (\quad)
 \end{aligned}$$

$$\begin{aligned}
 & \tilde{O} \quad \tilde{U} \quad \tilde{U} \quad \lambda_i \\
 & \tilde{O} \quad \tilde{O} \quad \tilde{O} \quad \tilde{O} \quad \tilde{U} \\
 & \tilde{O} \quad \tilde{O} \quad \tilde{O} \quad \tilde{O} \quad (12) \quad \tilde{U} \\
 & \quad \quad \quad \quad \quad \quad \quad \quad (3) \quad)
 \end{aligned}$$

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